# Right-to-left shunt has modest effects on CO<sub>2</sub> delivery to the gut during digestion, but compromises oxygen delivery

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# **ABSTRACT**

By virtue of their cardiovascular anatomy, reptiles and amphibians can shunt blood away from the pulmonary or systemic circuits, but the functional role of this characteristic trait remains unclear. It has been suggested that right-to-left (R-L) shunt (recirculation of systemic blood within the body) fuels the gastric mucosa with acidified and  $CO_2$ -rich blood to facilitate gastric acid secretion during digestion. However, in addition to elevating  $P_{CO2}$ , R-L shunt also reduces arterial  $O_2$  levels and would compromise  $O_2$  delivery during the increased metabolic state of digestion. Conversely, arterial  $P_{CO2}$  can also be elevated by lowering ventilation relative to metabolism (i.e. reducing the air-convection requirement, ACR). Based on a mathematical analysis of the relative roles of ACR and R-L shunt on  $O_2$  and  $CO_2$  levels, we predict that ventilatory modifications are much more effective for gastric  $CO_2$  supply with only modest effects on oxygen delivery. Conversely, elevating  $CO_2$  levels by means of R-L shunt would come at a cost of significant reductions in  $O_2$  levels. The different effects of altering ACR and R-L shunt on  $O_2$  and  $CO_2$  levels, is explained by the differences in the effective blood capacitance coefficients.

# **INTRODUCTION**

The ability to shunt blood away from the pulmonary or systemic circulations is a defining character of the reptilian and amphibian cardiovascular systems (Hicks, 1998). However, whilst much is known about the anatomical basis for central vascular shunts and their autonomic regulation, the functional role of bypassing one or the other circulations remains as mysterious as it is debated (Hicks and Wang, 2012). Thus, it remains uncertain as to whether this cardiovascular design is an exquisite adaptation to low ectothermic metabolism and intermittent pulmonary ventilation, or merely an atavistic relict with no particular functional benefits (Hicks and Wang, 2012).

In several species of reptiles and amphibians, the right-to-left (R-L) shunts (i.e. the direct recirculation of systemic venous blood into the arterial systemic circulation) decreases whenever oxygen demands are elevated (Hicks and Wang, 2012). However, in crocodilians, an elevated oxygen consumption associated with digestion may be an exception. A combination of unique anatomical features of the crocodilian cardiovascular system (Hicks, 1998) combined with physiological measurements fostered the idea that increased R-L shunts serves to fuel the gastric mucosa with acidic proton-rich blood during digestion in alligators (Farmer et al., 2008; Gardner et al., 2011; Jones and Shelton, 1993). Central to this proposal is the observation that the crocodilian coeliac artery appears as a continuation of the left aortic arch, which indicates that the stomach is preferentially perfused with CO<sub>2</sub>-rich blood from the right ventricle (*e.g.* (Jones, 1996; Webb, 1979)). In support for elevated (systemic) arterial partial pressure of CO<sub>2</sub> (Pco<sub>2</sub>) governing acid secretion, Farmer et al. (2008) reported slower digestion after surgical removal of the left aorta in alligators. However, a number of other studies show that growth is not affected by similar procedures (Eme et al., 2009; Eme et al., 2010), and it is possible that the slower digestion stems from reduced perfusion of the gastrointestinal organs after occlusion of the left aortic arch (Hicks and Wang, 2012).

Although the cardiovascular system must simultaneously provide for  $O_2$  delivery and  $CO_2$  removal, the proposition that R-L shunts assists gastric acid secretion has not included considerations of the inexorable reduction in  $O_2$  delivery. R-L shunts causes large reduction in arterial  $O_2$  levels – whether expressed as partial pressure,  $O_2$  concentration or haemoglobin saturation – (Wang and Hicks, 1996), while the effects on arterial  $P_{CO2}$  are predicted to be considerable smaller given the high capacitance coefficient for  $CO_2$  in blood. An increased R-L shunt during digestion would therefore also compromise oxygen delivery, which seems undesirable given the four-fold elevation in oxygen demands during digestion (Busk et al, 2000). In this context, it may be more prudent to elevate arterial  $P_{CO2}$  by means of ventilation (*i.e.* a lowering of the air convection requirement (ACR) for  $CO_2$ ), a response that has been suggested to compensate for the rise

in plasma bicarbonate during digestion (the so-called "alkaline tide"; (Hicks et al., 2000; Hicks and White, 1992; Wang et al., 2001b). However, decreasing the ACR to elevate  $CO_2$  levels will simultaneously lower the lung  $P_{O2}$  and could negatively impact oxygen delivery.

To address the compromise between adequate  $O_2$  delivery and arterial acid-base status, we developed an integrated numerical model that can be applied to amphibians and reptiles, to provide a quantitative comparison of the effects of R-L shunting and altered ventilation on blood  $O_2$  and  $CO_2$  levels.

# **MATERIALS AND METHODS**

Figure 1A illustrates the model of gas exchange for O<sub>2</sub> and CO<sub>2</sub> based on mass balances and relations that express electro-neutrality in blood compartments. The model does not include diffusion limitations or spatial heterogeneities at tissues or lungs, and incorporates a thermodynamically correct description of the Bohr-Haldane effect.

Mass balances

For O<sub>2</sub>:

$$\dot{V}_{O_2} = \dot{Q}_{sys}(C_{SaO_2} - C_{SvO_2})$$
 (1)

$$\dot{Q}_{pul} C_{PvO_2} + \dot{Q}_{RL} C_{PaO_2} = \dot{Q}_{sys} C_{SaO_2} + \dot{Q}_{LR} C_{SaO_2}$$
 (2)

$$Q_{sys}C_{SvO_{2}} + Q_{LR}C_{SaO_{2}} = Q_{RL}C_{PaO_{2}} + Q_{pul}C_{PaO_{2}}$$
 (3)

$$V_{A} \beta_{g} (P_{IO_{2}} - P_{AO_{2}}) = Q_{pul} (C_{PvO_{2}} - C_{PaO_{2}})$$
(4)

For CO<sub>2</sub>:

$$V_{CO_2} = Q_{svs}(C_{SvCO_3} - C_{SaCO_3})$$
 (5)

$$Q_{\text{pul}} C_{\text{PvCO}_2} + Q_{\text{RL}} C_{\text{PaCO}_2} = Q_{\text{sys}} C_{\text{SaCO}_2} + Q_{\text{LR}} C_{\text{SaCO}_2}$$
 (6)

$$\overset{\cdot}{Q}_{sys}C_{SvCO_{2}} + \overset{\cdot}{Q}_{LR}C_{SaCO_{2}} = \overset{\cdot}{Q}_{RL}C_{PaCO_{2}} + \overset{\cdot}{Q}_{pul}C_{PaCO_{2}}$$
 (7)

$$V_A \beta_g (P_{ACO_2} - P_{ICO_2}) = Q_{pul} (C_{PaCO_2} - C_{PvCO_2})$$
 (8)

See Table 1 and the list of symbols and abbreviations.

Concentrations and partial pressures in blood

The concentration of  $O_2$  in each blood compartment ( $C_{bO2}$ ) is the sum of haemoglobin bound  $O_2$  (product of blood Hb concentration ( $C_{Hb}$ ), number of  $O_2$  binding sites (q =4) and saturation ( $S_{O2}$ )) and the physically dissolved  $O_2$  (product of physical solubility ( $\alpha_{O2}$ ) and  $P_{O2}$ ):

$$C_{bO_2} = q C_{Hb} S_{O_2} + P_{O_2} \alpha_{O_2}$$
 (9)

To quantify the saturation of Hb with  $O_2$  and protons, the MWC two-state model (Monod et al., 1965) was incorporated where saturation is a function of both  $P_{O2}$  and proton concentration to include the Bohr/Haldane effect.

The total concentration of  $CO_2$  in blood ( $C_{bCO2}$ ) is the sum of the physically dissolved  $CO_2$  ( $\alpha_{CO2}$   $P_{CO2}$ ) and the bicarbonate and carbonate concentration, as quantified by the equilibrium constants of  $CO_2$  hydration ( $K_1$  and  $K_2$ ) and the proton concentration ([H<sup>+</sup>], which is related to  $S_{O2}$ ):

$$C_{bCO_2} = \alpha_{CO_2} P_{CO_2} \left( 1 + \frac{K_1}{[H^+]} + \frac{K_1 K_2}{[H^+]^2} \right)$$
 (10)

Electro-neutrality in blood

Equations that express electro-neutrality were derived by conservation of charge, where electro-neutrality in a given blood compartment (subscript i) is given below:

$$\left[ H^{+} \right]_{i} + SID = \frac{K_{w}}{\left[ H^{+} \right]_{i}} + \alpha_{CO_{2}} P_{CO_{2}i} \left( \frac{K_{1}}{\left[ H^{+} \right]_{i}} + \frac{2K_{1}K_{2}}{\left[ H^{+} \right]_{i}^{2}} \right) + \beta_{NB} \left( log(1/\left[ H^{+} \right]_{i}) - pH_{iso} \right) - pC_{Hb}S_{Hi}$$
(11)

SID is the strong-ion difference (Stewart, 1978),  $K_w$  is the ionic product of water,  $\beta_{NB}$  is the non-bicarbonate buffer capacity,  $pH_{iso}$  is the pH of zero net charge of the buffer groups.  $S_H$  is the fractional saturation of hemoglobin with protons and p is the number of Bohr-groups of haemoglobin.

Shunt fractions and blood flows

Total cardiac output  $(\dot{Q}_{tot})$  is the sum of pulmonary and systemic flows  $(\dot{Q}_{pul}$  and  $\dot{Q}_{sys}$ , respectively) and the

shunt flows ( $\dot{Q}_{RL}$  and  $\dot{Q}_{LR}$ ) are given by total blood flow and the shunt-fractions ( $F_{RL}=\dot{Q}_{RL}/\dot{Q}_{sys}$  and  $F_{LR}=\dot{Q}_{LR}/\dot{Q}_{sys}$  and  $F_{LR}=\dot{$ 

$$\dot{Q}_{pul} = \dot{Q}_{tot} \frac{1 - F_{RL}}{2 - F_{RI} - F_{IR}}$$
 (12)

$$\dot{Q}_{sys} = \dot{Q}_{tot} \left( 1 - \frac{1 - F_{RL}}{2 - F_{RL} - F_{LR}} \right)$$
 (13)

However, given the present purpose we only considered unidirectional R-L shunts.

### Numerical and analytical solutions

Due to the simplifying assumptions of the model, at steady state the pulmonary venous partial pressures of  $O_2$  and  $CO_2$  ( $P_{PVO2}$  and  $P_{PVCO2}$ ) is equal to the partial pressures in the lung ( $P_{AO2}$  and  $P_{ACO2}$ ). The total system of 12 equations that express mass balance and electro-neutrality with 12 dependent variables (*i.e.* partial pressures and proton concentrations in the systemic and pulmonary arterial and venous system for  $O_2$  and  $CO_2$ ) was solved numerically in Mathematica (v.10.3, Wolfram Research).

When blood capacitances of  $O_2$  and  $CO_2$  are assumed constant (approximately true for  $CO_2$  and applicable to  $O_2$  during hypoxia), the system of equations can be solved analytically leading to the following solutions:

$$\stackrel{\cdot}{V}_{O_2} R_{tot} = P_{IO_2} - P_{S_{VO_2}}$$
 (14)

$$\overset{\cdot}{V_{CO_2}} R_{tot} = P_{SvCO_2} - P_{ICO_2}, \tag{15}$$

where  $R_{tot}$  is the total resistance imposed to transport from the blood/tissues to the environment equal to the sum of the resistances associated with blood convective/perfusive transport ( $R_{perf}$ ) and ventilation ( $R_{vent}$ ):

$$R_{tot} = R_{perf} + R_{vent}$$
 (16)

When only considering unidirectional right-to-left shunts, the total resistance simplifies to:

$$R_{tot} = \frac{2 - F_{RL}}{Q_{tot} \beta_b (1 - F_{RL})} + \frac{1}{V_A \beta_g}$$
 (17)

, where  $\beta_b$  is the blood capacitance coefficient for  $O_2$  or  $CO_2$ . The left part on the right-hand side eq. (17) corresponds to  $(R_{perf})$  and simplifies to the normal perfusive resistance  $(1/(\sqrt[]{Q}_{tot} \beta_b))$  when there is no shunts, whereas the right part is  $R_{vent}$ . The perfusive resistance  $(R_{perf})$  can be expressed as the normal resistance without shunts  $(R_{perf\_FRL=0})$  multiplied by a function of the shunt fraction  $(i.e.\ f(F_{RL})=\frac{1}{2}(2-F_{RL})/(1-F_{RL}))$ :

$$R_{tot} = R_{perf E_{vr}=0} \cdot f(F_{RL}) + R_{vent}$$
(18)

While  $R_{vent}$  is the same for  $O_2$  and  $CO_2$ ,  $R_{perf}$  and hence  $R_{tot}$  differs given different  $\beta_b$ . The gas exchange limitation (Piiper and Scheid, 1972; Piiper and Scheid, 1981) imposed by R-L shunts( $L_{shunt}$ ) is given by one minus the total resistance without shunts ( $R_{tot}$ , where  $R_{RL}=0$ ) divided by the total resistance with shunts ( $R_{tot}$ ):

$$L_{shunt} = 1 - \frac{R_{totF_{RL}} = 0}{R_{tot}}$$

$$L_{shunt} = 1 - \frac{R_{perf F_{RL}} = 0}{R_{perf F_{RL}} = 0} \cdot f(F_{RL}) + R_{vent}$$
(19)

This can also be expressed by the dimensionless ratio of the normal perfusive to ventilatory resistance without shunts ( $\varphi$ ):

$$L_{shunt} = 1 - \frac{\varphi + 1}{\varphi \cdot f(F_{RL}) + 1}$$
 (20)

, where  $\phi$  is given by the ventilation to perfusion ratio and the blood gas partitioning coefficient ( $\lambda = \beta_b/\beta_g$ ) as follows:

$$\varphi = \frac{R_{\text{perf } F_{RL}=0}}{R_{\text{vent}}} = \frac{V_A}{\sqrt{Q_{\text{tot}}}} \frac{1}{\lambda}$$
 (21)

From eq. (20) it is given that the transport limitation imposed by shunts approach zero when  $\phi$  approach zero (*i.e.* infinitely high blood flow and partitioning coefficient relative to ventilation). Conversely, the limitation approaches  $F_{RL}/(2-F_{RL})$  when  $\phi$  approaches infinity (*i.e.* infinitely high ventilation and low partitioning coefficient relative to blood flow).

#### **RESULTS AND DISCUSSION**

The isolated and combined effects of R-L shunts and ACR are illustrated in 3D plots in Figures 1B-D where arterial  $P_{CO2}$ ,  $P_{O2}$  and  $HbO_2$  saturation ( $S_{O2}$ ) are shown as functions of both R-L shunt fraction ( $F_{RL}$ ) and alveolar ventilation. It is immediate clear that arterial  $P_{CO2}$  increases most steeply when alveolar ventilation is reduced (*i.e.* reduced ACR), but only moderately when  $F_{RL}$  is increased (Fig. 1B). Conversely, both arterial  $P_{O2}$  and  $S_{O2}$  are markedly reduced as the R-L shunt increases, whilst reductions in alveolar ventilation only moderately reduce  $S_{O2}$  (Figs. 1C,D). Thus, our theoretical analysis reveals substantial differences on the influence of R-L shunt and ACR on arterial blood gases, and predicts that ventilatory compensations are much more effective in altering arterial  $P_{CO2}$  than cardiac shunt patterns.

The differences in the behaviours of  $O_2$  and  $CO_2$  upon changing shunt pattern or ACR are also illustrated in Figure 2A-D that shows  $P_{02}$ - $P_{CO2}$  diagrams and similar plots that relate  $P_{CO2}$  and  $S_{O2}$ . In Figure 2B, the dashed line describes steady-state solutions for lung gases and hence also the arterial blood gases in the absence of cardiac shunts (*i.e.* the mammalian condition). In this case, reductions in ACR cause similar, but reciprocal changes in arterial  $P_{O2}$  and  $P_{CO2}$  as predicted by RQ (set to 1 in the simulations). Conversely, an introduction of R-L shunt at a given ACR cause large reductions in arterial  $P_{O2}$  while arterial  $P_{CO2}$  only increases moderately (full green curve in Fig. 2B). Thus, to produce the same elevation in arterial  $P_{CO2}$  by means of R-L shunt as by a moderate reduction in ACR (*e.g.* a reduction from 28 to 20 mL air/mLCO<sub>2</sub>; Fig. 2B), the shunt fraction would have to increase to 0.8, meaning that 80% of the systemic venous return bypasses the lungs (Fig. 2B). Such a large shunt fraction would concomitantly reduce arterial  $P_{O2}$  from more than 120 mmHg to less than 30 mmHg (Fig. 2B) and a reduction in  $S_{O2}$  from around 1.0 to less than 0.5 (Fig 2A).

The complete solutions for different combinations of  $F_{RL}$  (varied 0-0.8) and ACR (varied 12.5-50) for arterial blood are given in Figures 2C and D. The colour coding indicates increasing  $P_{CO2}$  and the thicker lines originating from the air-line (the black dashed line/curve) depict how  $P_{O2}$ ,  $P_{CO2}$  and  $S_{O2}$  change as  $F_{RL}$  is altered at several constant levels of ACR. The thinner curves, originating from the thicker blood curves, represents solutions when ACR is altered at a given constant  $F_{RL}$ . By combining the horizontal axes of Figures 2C and D, the possible solutions are summarized as a 3D diagram with  $P_{CO2}$  on the vertical z-axis and  $S_{O2}$  and  $P_{O2}$  on the horizontal x and y-axes (Fig. 2E). In this representation, the horizontal x-y plane reflects the effective  $O_2$  equilibrium curve. Figure 2E illustrates that increasing  $F_{RL}$  causes large reductions in  $P_{O2}$  of the arterial and venous blood along the  $O_2$  equilibrium curve leading to pronounced  $S_{O2}$  reduction with only moderate elevation of  $P_{CO2}$ . Conversely, reducing ACR at a given  $F_{RL}$  leads to a large elevation of  $P_{CO2}$  with only moderate reductions in  $S_{O2}$  (thinner upwards bending curves in Fig. 2E).

The different effects of altering ACR and R-L shunt on  $O_2$  and  $CO_2$  is explained by the differences in blood capacitance coefficients ( $\beta_b$ ) (alternatively expressed as differences in blood gas partitioning coefficients,  $\lambda$ ). This is illustrated in Figure 3, showing the limitation imposed on gas exchange by  $F_{RL}$  (eq. (21)). Here the ratio of the normal perfusive to ventilatory resistance without shunts ( $\phi$ ) is varied from a physiologically relevant range for  $O_2$  and  $CO_2$  (colour coded) and the asymptotic relation between the limitation and  $F_{RL}$  for  $\phi$  approaching infinity and  $\phi$ = 0 is given by the black curve and the horizontal axis. Figure 3 emphasizes that at a given shunt fraction, the gas species mostly limited by the shunt is the one with the highest blood to air convective resistance ( $\phi$ ) and hence the lowest  $\lambda$  (*i.e.* lowest  $\beta_b$ ). Therefore, due to the high  $\beta_b$ ,  $CO_2$  is less limited by shunts than  $O_2$  although the differences may become less distinct in deep hypoxia where the effective  $\beta_b$  for  $O_2$  increases. The same conclusion was made by Wagner when considering the effects of lung shunts on  $O_2$  vs.  $CO_2$  exchange (Wagner, 1979). Besides the differences in effects of shunts on  $O_2$  and  $CO_2$ , Figure 3 also illustrates that the limitation in general is predicted to increase when overall  $V_A/\dot{Q}_{tot}$  is high and vice versa.

If digestion is facilitated by supplying the gut with blood with higher  $CO_2$  levels, our model predicts that this is best mediated by reducing ACR instead of increasing R-L shunt. Elevating  $CO_2$  levels by increasing R-L shunt would come at the cost of pronounced reductions in  $O_2$  levels producing hypoxemia at a time where  $O_2$  demand may be elevated four-fold above resting (e.g. (Busk et al., 2000)). Conversely, reductions of ACR entail much smaller reductions in  $O_2$  delivery, but provides for an effective elevation of  $P_{CO2}$  that compensates for the alkaline tide during digestion (Wang et al., 2001a). Furthermore, these postprandial reductions in ACR are well-known in reptiles (Hicks et al., 2000; Overgaard et al., 1999; Secor et al., 2000) and  $P_{O2}$  remains high during digestion in all animals studied, including alligators (Busk et al., 2000; Hartzler et al., 2006; Overgaard et al., 1999).

For many reptiles and amphibians, digestion is associated with large elevations in oxygen demands and an increased need to secrete gastric acid with resulting challenges to blood acid-base balance. Our theoretical approach clearly demonstrates that reliance on R-L shunting to meet the digestive demands conflicts significantly with increased metabolic demands of the digestive organs, and cannot provide adequate compensation for the alkaline tide. In contrast, ventilatory regulation, through reductions in ACR, addresses all the physiological challenges simultaneously, i.e. blood-acid base regulation, increased CO<sub>2</sub> delivery to the gastric mucosa without sacrificing oxygen delivery. Thus, while our theoretical model obviously does not provide information on the actual physiological responses of living animals, it would certainly seem that natural selection should favour efficient ventilatory regulation on arterial P<sub>CO2</sub> rather than the ineffective mean of regulation by central vascular shunts.

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#### **Author Contributions**

This analysis results from numerous discussions over the past decade involving all the authors. C.L.M. constructed the model used in the manuscript on the basis of previous simpler attempts. The manuscript was written by H.M. and T.W. with continuous input and final approval of all co-authors.

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# List of symbols and abbreviations not appearing in Table 1

ACR Air convection requirement

R-L shunt Right-to-left shunts; i.e. the recirculation of systemic venous blood in the systemic

circulation

 $P_{CO2}$ ,  $P_{O2}$  Partial pressure of  $CO_2$  or  $O_2$  in a given compartment  $C_{SaCO2}$ ,  $C_{SaO2}$  Concentration of  $CO_2$  or  $O_2$  in the systemic arterial blood

C<sub>PvCO2</sub>, C<sub>PvO2</sub> Concentration of CO<sub>2</sub> or O<sub>2</sub> in pulmonary venous return (i.e. left atrium)

 $C_{PaCO2}$ ,  $C_{PaO2}$  Concentration of  $CO_2$  or  $O_2$  in the pulmonary artery

 $C_{SVCO2}$ ,  $C_{SVO2}$  Concentration of  $CO_2$  or  $O_2$  in systemic venous return (i.e. right atrium)

 $P_{ACO2}$ ,  $P_{AO2}$  Partial pressure of  $CO_2$  or  $O_2$  in the lung gas  $P_{ICO2}$ ,  $P_{IO2}$  Inspired partial pressure of  $CO_2$  or  $O_2$ 

 $\begin{array}{lll} Q_{tot} & Total \ cardiac \ output \\ \dot{Q}_{pul} & Pulmonary \ blood \ flow \\ \dot{Q}_{sys}, & Systemic \ blood \ flow \\ \dot{Q}_{RL} & Right \ to \ left \ shunt \ flow \\ \dot{Q}_{LR} & Left \ to \ right \ shunt \ flow \\ S_{O2} & Haemoglobin \ O_2 \ saturation \end{array}$ 

S<sub>H</sub> Fractional saturation of hemoglobin with protons

p Number of Bohr-groups of hemoglobin

λ Blood/gas partitioning coefficient

R<sub>tot</sub> Total resistance imposed to transport between tissues and the environment

R<sub>perf</sub> Blood convective/perfusive resistance R<sub>vent</sub> Air convective/ventilatory resistance

L<sub>shunt</sub> Gas exchange limitation imposed by shunts

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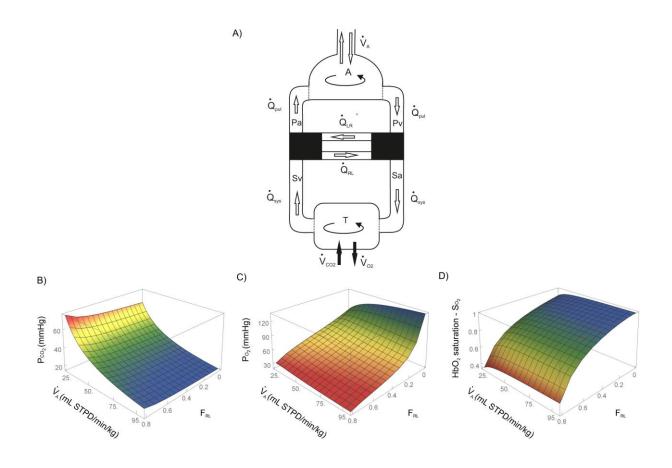
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# Table

Table 1

Parameters and variables	Abbreviat ion	Value	Reference
Mean alveolar/effective ventilation	V <sub>A</sub>	Varied: 25-100 mLSTPD min <sup>-1</sup> kg <sup>-1</sup>	
Lung air capacitance coefficient	$\beta_g$	1/730 mLSTPD mL <sup>-1</sup> mmHg <sup>-1</sup>	
Total cardiac output	Q <sub>ot</sub>	150 mL min <sup>-1</sup> kg <sup>-1</sup>	
Right to left shunt fraction	F <sub>RL</sub>	Varied: 0.0-0.8	
Left to Right shunt fraction	F <sub>LR</sub>	0	
Blood non-bicarbonate buffer capacity excluding the contribution from Hb Bohr-groups	βΝΒ	10.08 mM/pHUnit	Leads to similar total non-bicarbonate buffer capacity as reported for turtles (Weinstein et al., 1986)
Strong ion difference	SID	11.42 mM	Value required for initial condition of P <sub>CO2</sub> =35 mmHg, P <sub>O2</sub> =100 mmHg, pH=7.2
Haemoglobin concentration	Снь	1.25 mM	Half of typical human value
Midpoint for pK	pK <sub>m</sub>	7.3	Similar to human value
Isoelectric pH value for haemoglobin	pH <sub>iso</sub>	7.2	Similar to human value
Physical solubility of O <sub>2</sub> in blood	α <sub>02</sub>	0.00125 mM mmHg <sup>-1</sup>	(Christoforides and Hedley-Whyte, 1969)
Physical solubility of CO <sub>2</sub> in blood	α <sub>CO2</sub>	0.032135 mM mmHg <sup>-1</sup>	(Reeves, 1976)
CO <sub>2</sub> production and O <sub>2</sub> consumption	 V <sub>CO2</sub> , V <sub>O2</sub>	2 mL STPD min <sup>-1</sup> kg <sup>-1</sup>	

# **Figures**



**Figure 1.** Panel A illustrates the compartment model with abbreviations as follows: T: tissues, Sv: systemic venous blood, Pa: pulmonary arterial blood, A: lung, Pv: pulmonary venous blood, Sa: systemic arterial blood. For other symbols see List of abbreviation and Table 1. The 3D plots in panels B-D illustrate how (systemic) arterial  $P_{CO2}$ ,  $P_{O2}$  and haemoglobin  $O_2$  saturation ( $S_{O2}$ ), change as a function of the alveolar ventilation (and hence air-convection requirement, ACR) and the right-to-left shunt fraction ( $F_{RL}$ ).

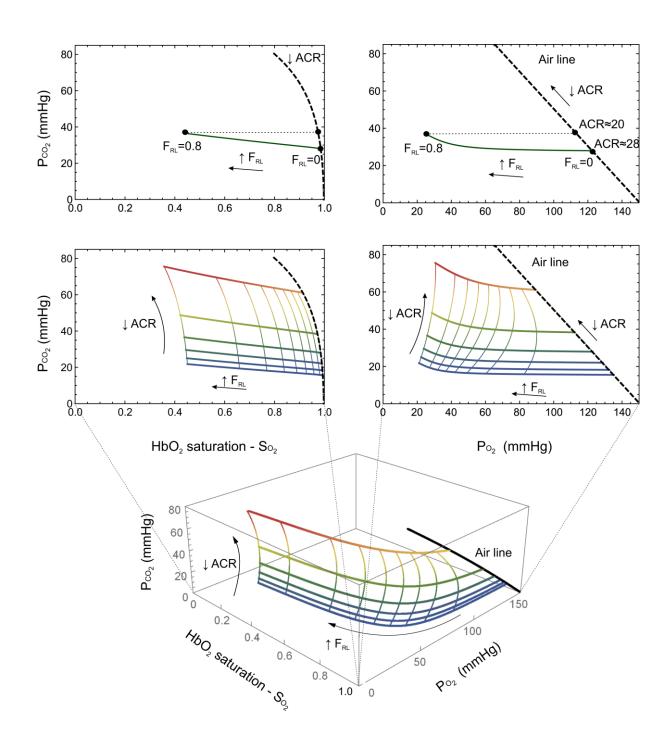
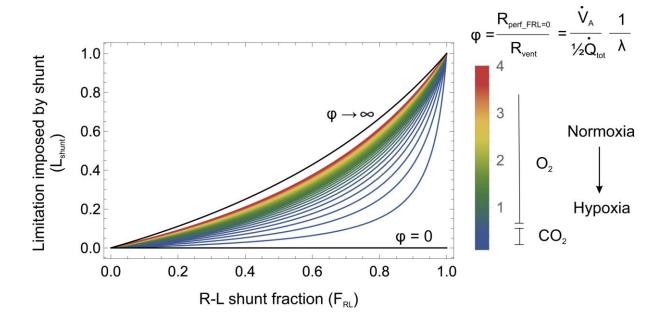


Figure 2. Panel A-D shows arterial  $P_{CO2}$  as a function of either haemoglobin  $O_2$  saturation ( $S_{O2}$ ) (panels A and C) or  $P_{O2}$  (panels B and D). In panels B and D the dashed black line is the air-line with a slope given by RQ

that describes how P<sub>CO2</sub>and P<sub>O2</sub>change when altering air-convection requirement (ACR) without shunts and similarly in panels A,C where the "air-line" becomes a curve. In panel B, the thick green curve originating at the dashed air-line/curve shows solutions when the right-to-left shunt fraction (FRL) is increased at a constant ACR. Notice that in order to produce the same elevation in arterial P<sub>CO2</sub> by means of R-L shunt as by a moderate reduction in ACR (e.g. a reduction from 28 to 20 mL air/mLCO<sub>2</sub>), the shunt fraction would have to increase to 0.8 with a concomitant large reduction in arterial P<sub>02</sub> and S<sub>02</sub> (panel A). Panel C and D illustrate solutions for different combinations of F<sub>RL</sub> (varied 0-0.8) and ACR (varied 12.5-50 mL air/mLCO<sub>2</sub>) where the colour coding indicates increasing Pco2. Here the thicker curves originating from the airline/curve shows the effects of altering F<sub>RL</sub> at a given constant ACR. Conversely, the thinner curves originating from the thicker curves show the effects of altering ACR at a given F<sub>RL</sub>. The 3D plot in panel E is a combination of panel C and D where P<sub>CO2</sub> is on the vertical z-axis and S<sub>O2</sub> and P<sub>O2</sub> is on the horizontal x and y-axes and therefore also illustrates the effective O<sub>2</sub> equilibrium curve. Panel E summarizes the effects of altering F<sub>RL</sub> (thicker curves) and ACR (thinner curves) on both (systemic) venous and arterial blood. Notice that when increasing F<sub>RL</sub> at a given ACR, the arterial and venous points move down the O₂ equilibrium curve with only small elevations in Pco2. Conversely, reducing ACR at a given shunt leads to pronounced elevations of P<sub>CO2</sub> but only moderate reductions in S<sub>O2</sub>.



**Figure 3.** Simplified analytic solution of the model that illustrates the limitation imposed on gas exchange by shunts (L<sub>shunt</sub>, eq. (21)) as a function of the right-to-left shunt fraction (F<sub>RL</sub>) for different values of the ratio of the perfusive to ventilatory resistance without shunts ( $\phi$ , eq. (22), colour coded). Notice that the asymptotic limitations when  $\phi$  approach infinity or zero is plotted. As a consequence of higher blood capacitance coefficient ( $\beta$ <sub>b</sub>) and hence blood/gas partitioning coefficient ( $\lambda$ ),  $\phi$  for O<sub>2</sub> is higher than for CO<sub>2</sub> and hence O<sub>2</sub> uptake will be more limited by a given shunt.