## Locomotor patterns change over time when exposed to an uneven surface

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## Summary statement

We show that the movement strategies of unimpaired adults when walking on uneven terrain adapt over time with longer exposure to the surface.


#### Abstract

During walking, uneven surfaces impose new demands for controlling balance and forward progression at each step. It is unknown the extent to which walking may be refined given a level of stride-to-stride unpredictability at distal level. Here, we explored the effects of an uneven terrain surface on whole-body locomotor dynamics on immediate exposure and after a familiarization period.

Eleven young, unimpaired adults walked for 12 minutes on flat and uneven terrain treadmills. The whole-body center of mass excursion range ( $\mathrm{COM}_{\mathrm{EXc}}$ ) and peak velocity ( $\mathrm{COM}_{\text {VEL }}$ ), step length and width were estimated. On first exposure to uneven terrain, we saw significant increases in lateral $\mathrm{COM}_{\mathrm{EXC}}$ and $\mathrm{COM}_{\mathrm{VEL}}$, and in the variability of $\mathrm{COM}_{\mathrm{EXC}}$, COM Vel and foot placement in both anterior-posterior and medial-lateral directions. Increases in step width and decreases in step length supported the immediate adoption of a cautious, restrictive solution on uneven terrain. After familiarization, step length increased and the variability of anterior-posterior COMvel and step length reduced, while in the medial-lateral direction step width and COMvel reduced, alluding to a refinement of movement and a reduction of conservative strategies over time. The variability of medial-lateral COMEXc and COMvEL increased, however, consistent with a release of previously constrained degrees of freedom. Despite this increase in variability, a strong relationship between step width and medial-lateral COM movement was maintained.

Our results indicate that movement strategies of unimpaired adults when walking on uneven terrain can evolve over time with longer exposure to the surface.


## Introduction

The urban environment is rarely completely level, therefore mobility outside the home presents unpredictability that can challenge locomotion if it is not sufficiently adaptable (Patla and Shumway-Cook, 1999). The multiple joints of the uncompromised musculoskeletal system provide a huge amount of flexibility, and enable gross functional movements, such as a step, to be produced by infinite combinations of trajectories of the individual segments of the body, e.g. shank, thigh, foot (Bernstein, 1967; Fitts, 1964). Balance during walking is dependent on the appropriate orchestration of segments such that the movement of their combined center of mass (COM) is maintained within a functional boundary related to foot position (Hof et al., 2005), regardless of context (Courtine and Schieppati, 2004; Patla and Shumway-Cook, 1999; Patla, 2003).

During walking, segments are loosely organized into patterns that are similar from stride to stride. Even on level ground these patterns are never identical, however, reflecting an ability to exploit system redundancy, without which gait would appear robotic (Harbourne and Stergiou, 2009; Harrison and Stergiou, 2015; Stergiou and Decker, 2011; van Emmerik and van Wegen, 2000). Hypothetically, upon a consistent support surface and assuming negligible additional external force on the body, an identically produced step would have an identical result following contact with the ground. Further, the dynamic consequences of the interaction between the body and the ground would be largely predictable, and the surface could be readily exploited to facilitate the task (see, e.g. Fajen et al., 2009). When the contour of the ground fluctuates, however, a new control problem is presented. The reaction forces experienced by the body via the foot will vary in magnitude and direction from stride to stride, subtly or markedly changing the demands of forward progression and dynamic balance (Patla and Shumway-Cook, 1999; Patla, 2003). Peaks and troughs may act to impair or accelerate the rotation of the leg about the ankle in the direction of walking, inducing delayed or early foot contacts in the other limb. Contours that act to invert or evert the foot will encourage medial or lateral movement of the body whilst shifting the boundary and integrity of the base of support provided by the feet (Patla, 2003). A step that is identically produced by an individual cannot physically produce an identical result; to achieve kinematic uniformity from stride to stride would require the adjustment of internally produced forces, to counteract the changes in ground reaction force experienced.

Healthy, unimpaired adults are able to walk without loss of balance on unstable and unpredictable surfaces, although they display increases in step length and width variability, and greater and more variable whole-body center of mass excursions, velocities and accelerations during walking (see e.g. Gates et al., 2012; Richardson et al., 2005; Stokes et al., 2017; Thies et al., 2005; Voloshina et al., 2013). As the prevention of loss of balance relies on maintaining the relationship between the base of support and COM movement (Hof et al., 2005; Pai and Patton, 1997), unpredictable dynamics induced by an uneven walking surface may present an increased and ongoing risk of a loss of balance occurring.

Foot placement during unperturbed gait has been shown to be closely attuned to movement of the center of mass, as estimated from the pelvis or trunk (Arvin et al., 2016; Arvin et al., 2018; Roden-Reynolds et al., 2015; Wang and Srinivasan, 2014). Lateral foot positioning, for example, can be predicted from the velocity and position of the pelvis or whole-body center of mass (Arvin et al., 2018; Wang and Srinivasan, 2014). This coupling appears to hold during isolated and unpredictable lateral perturbations directed at the waist (Hof and Duysens, 2013) and at the foot (Rankin et al., 2014), and empirical evidence points to a neuromechanical control strategy involving the proprioception (Arvin et al., 2016; Roden-Reynolds et al., 2015) and action of the hip abductors (Roden-Reynolds et al., 2015).

In addition to this proposed neuromechanical coupling mechanism (Roden-Reynolds et al., 2015), commonly reported gross deviations in the presence of balance challenges include decreasing step length to permit a flatter foot contact with the ground (Gates et al., 2012); increasing double support time (Menant et al., 2009) thereby reducing the period when the body is unilaterally supported; increasing knee and hip flexion during swing to avoid tripping (Gates et al., 2012); and increasing step width to increase the boundary within which the COM may safely deviate without risk of a sideways fall (Hak et al., 2013; Rankin et al., 2014). Such strategies would reduce the likelihood of any unpredictable encounter causing excessive divergence of the COM with respect to the base of support, and may be conservative solutions to the unpredictability problem.

Although these strategies may be effective for maintaining balance, they may not constitute the most functional way of moving through the environment. For example, highly variable trunk and head movement, a lack of movement fluidity, or the requirement for greater attention to be directed towards walking may disrupt the performance of concurrent tasks
(Ebersbach et al., 1995), and increases in step width have been shown to increase metabolic cost by over $40 \%$ (Donelan et al., 2001). These results suggest that, although adaptations to account for terrain are well within the capability of young adults, they can result in reduced locomotor economy (Voloshina et al., 2013) and can be detrimental to the effectiveness of walking as a means to travel from one place to another. As such, refinement may be beneficial.

Previous studies exploring movement on uneven ground have focused only on isolated bouts of walking (e.g. Gates et al., 2012; Richardson et al., 2005; Thies et al., 2005), primarily via traverses of a section of an uneven surface within the laboratory environment. Voloshina et al. (2013) utilized a treadmill with an adapted belt to explore mechanics and energetics on uneven ground, permitting a longer period of continuous walking to be evaluated. The study, however, focused only on the final 2.5 minutes of a 10 -minute trial. It therefore remains unknown whether people can refine their movement on uneven ground over time. It might be expected that conservative strategies would be employed on uneven ground on first encounter to avoid falls, but adjusted with familiarity to optimize movement based on a greater awareness of the constraints and challenges of the terrain underfoot.

The purpose of this study was to investigate the effect of terrain unevenness on the whole-body locomotor dynamics of unimpaired individuals. Specifically, we examined walking both on first exposure to uneven ground, and after a period of familiarization, with a focus on center of mass movement and foot placement from stride to stride. We hypothesized that on first exposure to an uneven terrain surface we would observe an increase in the amount of variability in step patterns (length and width) and COM dynamics, accompanied by increases in whole-body COM excursion and peak COM velocity on a step-to-step basis. We predicted that unimpaired individuals would adopt a restrictive and cautious solution at first; specifically, a reduction in step length and an increase in step width, to mitigate the risk of a loss of balance when first encountering the surface. It was also anticipated that, given their adaptability, individuals would refine their solution with time leading to a reduction in COM movement, the amount of variability, and these potentially costly or effortful conservative step placement strategies.

## Materials and methods

## Participants

Eleven young unimpaired adults (mean $\pm \mathrm{sd} ; 24.4 \pm 2.8$ years, $78.3 \pm 10.1 \mathrm{~kg}, 1.79 \pm 0.09$ m) were recruited from the staff and student body of the University of Nebraska at Omaha and provided written informed consent to participate. Sample size was based on a power analysis indicating that an effect size of 0.8 could be achieved with $80 \%$ power at $\alpha=0.05$ and 10 participants. The study protocol was approved by the University of Nebraska Medical Center Institutional Review Board. All participants were familiar with treadmill walking or running and reported themselves able to walk for at least 30 minutes continuously with no perceived fatigue. They had no history of ankle instability, knee ligamentous injury or knee instability; no diagnosed joint laxity or hypermobility; no lower limb osteoarthritis; no current musculoskeletal injury or pain; no musculoskeletal and neurological disorder; had sustained no lower limb injury in the previous 12 months nor had had surgery in the previous 6 months; had no history of cardiovascular events; and were not pregnant.

## Procedures

A tight athletic suit was worn for motion capture purposes. Participants were tested wearing flexible footwear provided by the laboratory. A 6-degrees-of-freedom full-body marker set based on Calibrated Anatomical Systems Technique (Cappozzo et al., 1995) was applied, with motion capture markers affixed to the feet, lower leg, thigh, pelvis, trunk, shoulders, arms, hands and head (see supplementary information). Five minutes of walking were completed on a standard flat-belt commercial treadmill (TRM 731, Precor, Woodinville, WA, USA) prior to the start of the captured trials in order to familiarize the participants with the footwear, equipment and environment.

Walking trials were performed on the flat terrain treadmill and on an in-house modified uneven terrain treadmill (Figure 1). The treadmill belt width and average height were consistent across devices, and participants were asked to focus on a fixation cross mounted at the same height from the belt on the front of each, to maintain visual consistency across walking conditions. A ceiling-mounted harness was worn for all trials for safety.

All trials were performed at a fixed speed of $1 \mathrm{~m} / \mathrm{s}$, consistent with previous literature (Voloshina et al., 2013) and determined to be comfortable on the uneven terrain previously in a
group of 17 healthy adults. In order to avoid familiarization with the uneven terrain surface during treadmill acceleration at the start of the trial, participants were asked to straddle the walking surface until the belt was at speed, then to step on and immediately remove their hands from the handrails. Participants walked for 12 minutes on flat terrain followed by 12 minutes on uneven terrain, with a break of at least 5 minutes between trials. Kinematic data were captured at 100 Hz using a 17-camera motion capture system (Motion Analysis Corp., Santa Rosa, CA, USA).

## Outcome variables

Subsequent variables selected for analysis focused on whole-body measures of gait performance and balance; COM excursion range ( $\mathrm{COM}_{\mathrm{EXC}}$ ) and velocity (COM VEL) in the anterior-posterior and medial-lateral directions, and step length and step width to represent foot placement in anterior-posterior and medial-lateral directions respectively (Figure 2). Analyses were performed under the assumption that treadmill walking was already a learned skill. Baseline level walking data were extracted from the final 60 strides of the flat terrain trial (FT), at which point participants would have completed 15-16 minutes of walking in total to enable familiarization to the set treadmill speed, footwear, harness and environment; isolating the effect of the terrain. Values of each variable were calculated from 60 strides on each limb at the start and end of the uneven terrain trial (UT1, UT2 respectively). This is with the exception of one participant who stumbled briefly due to a toe catch during UT1. For this participant, three strides were excluded bilaterally, with recovery visually determined from video and motion capture data based on trunk and foot movement. The mean and standard deviation of the COM anteriorposterior (AP) excursion range during each step (COMEXC-AP and variability of COMEXC-AP respectively), the maximum anterior velocity during each step (COMvel-ANT, variability of COMvel-ANT), and the step length were calculated and extracted. In the direction perpendicular to the plane of progression, the mean and standard deviation of the center of mass medial-lateral (ML) excursion range during each step (COMExc-ML, variability of COMExc-ML), the maximum lateral velocity (directed towards the stance leg) during each step (COM VEL-LAT, variability of $\mathrm{COM}_{\mathrm{VEL}}-\mathrm{LAT}$ ), and the step width were calculated (Figure 2).

## Processing and data extraction

Kinematic data were tracked in Cortex (Motion Analysis Corp, Santa Rosa, CA, USA) with further processing undertaken in Visual3D (C-Motion Inc., Germantown, MD, USA). The full-body 6-degrees-of-freedom model was applied, comprised of 15 segments: bilateral feet, shanks, thighs, upper arms, forearms and hands, and head, trunk and pelvis (see supplementary information). Segment masses were computed relative to body mass, according to Dempster (Dempster, 1955) and center of gravity locations estimated based on geometric shape approximations of each segment (cylinder, cone, ellipsoid; (Hanavan, 1964); see supplementary for full description of biomechanical model). Foot mass was adjusted to account for footwear. A 4th-order low pass Butterworth filter was applied to raw marker data. Cut off frequencies were determined using power spectral analysis as described by Winter (Giakas, 2004; Winter, 2009) and ranged from 7 Hz (head) to 12 Hz (feet).

To identify the terrain contour beneath each footfall and ensure that no changes to the task occurred due to systematic changes in foot placement across trials, the range and standard deviation of the sagittal and coronal plane midstance foot angles were calculated. These were extracted for each step; defined as the instantaneous angle of the foot with respect to the laboratory coordinate system at the time point at which the contralateral swing foot toe marker (placed dorsal to the second metatarsal head) crossed the stance foot heel marker. The appropriateness of utilizing this toe-heel crossing instance to determine ground contour was verified using video data. Visual inspection confirmed that no participant adopted an early plantarflexion vaulting strategy and indicated that both the posture of the foot and the slope of the ground beneath it could be adequately characterized at this instance.

Variables were computed for both limbs and categorized according to the limb each participant reported they would kick a ball with, designated as their dominant limb. Foot contact events were estimated using a kinematic velocity-based algorithm (Zeni et al., 2008), and the location of foot contact at the start of each gait cycle was approximated by the position of the ankle joint center. Step length was defined as the distance in the treadmill direction of travel between the ipsilateral and previous contralateral foot contact locations plus the distance the treadmill belt travelled within that step duration (Jordan et al., 2007). Step width was defined as the distance perpendicular to the direction of travel between consecutive foot contact locations.

Trial order was not randomized in order to avoid potential carryover effects following walking on the uneven ground.

## Statistical analysis

Shapiro-Wilk tests and Q-Q plots were initially used to evaluate normality for each variable. In order to test the hypotheses that (1) there would be an increase in the amount of variability in step patterns and a more restrictive and cautious solution on first exposure to uneven terrain, and that (2) movement would be refined over time, each variable ( $\mathrm{COM}_{\mathrm{EXc}}-\mathrm{AP}$, variability of $\mathrm{COM}_{\mathrm{ExC}}-\mathrm{AP}, \mathrm{COM}_{\mathrm{EXC}}-\mathrm{ML}$, variability of $\mathrm{COM}_{\mathrm{EXC}}-\mathrm{ML}, \mathrm{COM}$ VEL-ANT, variability of COMVEL-ANT, COMVEL-LAT, variability of COMVEL-LAT, step length, step length variability, step width, step width variability, plus sagittal and coronal plane midstance foot angle) was examined using a 1-way repeated measures ANOVA (3 levels: FT, UT1, UT2). Friedman tests (3 levels: FT, UT1, UT2) were used for variables that were not non-normally distributed. Where differences were identified, Tukey's HSD and Wilcoxon signed rank tests were applied, for normally and non-normally distributed variables respectively.

## Results

All participants were able to complete walking trials without the use of the handrails. Only the (self-reported) dominant limb results are reported below as similar trends were observed for both limbs.

Midstance foot angle range was significantly different across walking bouts in both sagittal $\left(\mathrm{F}_{2,20}=133.201, \mathrm{p}<0.001\right)$ and coronal planes $\left(\mathrm{F}_{2,20}=250.983, \mathrm{p}<0.001\right.$; Table 1$)$. The range was higher in both uneven terrain walking bouts in comparison to flat terrain (all comparisons $\mathrm{p}<0.01$ ) but there was no significant difference between UT1 and UT2 ( $\mathrm{p}>0.05$ ). Significant differences were observed in the standard deviation of mid stance foot angle (Sagittal $-\mathrm{F}_{2,20}=152.926, \mathrm{p}<0.001$; Coronal $-\mathrm{F}_{2,20}=231.588, \mathrm{p}<0.001$ ). Post hoc tests revealed that differences occurred only between FT and UT1, and FT and UT2 (all comparisons p < 0.01). The range and standard deviation of foot positions when the foot was loaded, which were 3-7 times greater than those observed during level walking, indicate that the surface of the treadmill used for the study successfully affected distal extremity posture from stride to stride, with the potential to alter level walking patterns (Klint et al., 2008).

## Anterior-Posterior dynamics

COM ${ }_{\text {EXC }}-\mathrm{AP}\left(\mathrm{F}_{2,20}=7.053, \mathrm{p}=0.005\right)$ and variability of $\mathrm{COM}_{\mathrm{EXC}}-\mathrm{AP}\left(\mathrm{F}_{2,20}=15.374, \mathrm{p}<\right.$ 0.001 ) were significantly different across walking bouts (Figure 3A). Post-hoc tests revealed that COMEXC-AP was higher on UT2 in comparison to FT (p $<0.01$ ) only. Variability of COMEXCAP increased on UT1 ( $\mathrm{p}<0.01$ ) and but there was no further change at UT2 ( $\mathrm{p}>0.05$ ).

COMyEL-ANT did not change across walking bouts $\left(\chi^{2}{ }_{2}=5.636, p=0.06\right)$. Significant differences in variability of COMvel-ANT were observed ( $\mathrm{F}_{2,20}=74.868$, $\mathrm{p}<0.001$ ) with post hoc tests revealing a higher variability on UT1 in comparison to FT (p < 0.01; Figure 3B). Variability of COMVEL-ANT reduced at UT2 ( $\mathrm{p}<0.01$ ) but remained higher than FT ( $\mathrm{p}<0.01$ ).

Significant differences in step length $\left(\mathrm{F}_{2,20}=21.738, \mathrm{p}<0.001\right)$ and step length variability $\left(\mathrm{F}_{2,20}=26.062, \mathrm{p}<0.001\right)$ were observed across walking bouts (Figure 3C). Step length was on average lower on UT1 than FT ( $\mathrm{p}<0.01$ ), increased at UT2 ( $\mathrm{p}<0.05$ ) but remained shorter on average than FT ( $p<0.01$ ). Step length variability was higher at UT1 in comparison to FT ( $\mathrm{p}<0.01$ ). It then reduced at UT2 ( $\mathrm{p}<0.05$ ), although remained significantly different to FT $(\mathrm{p}<0.01)$.

## Medial-lateral dynamics

There were significant differences in both $\operatorname{COM}_{\mathrm{EXc}}-\mathrm{ML}\left(\mathrm{F}_{2,20}=13.673, \mathrm{p}<0.001\right)$ and variability of $\mathrm{COM}_{\mathrm{EXC}}-\mathrm{ML}\left(\mathrm{F}_{2,20}=26.589, \mathrm{p}<0.001\right)$ (Figure 4A). Post hoc tests revealed a significantly higher COMExc-ML at UT1 in comparison to FT ( $\mathrm{p}<0.01$ ) and UT2 in comparison to FT ( $\mathrm{p}<0.01$ ), but not between UT1 and UT2 ( $\mathrm{p}>0.05$ ). Variability of COMExc-ML was greater on UT1 ( $\mathrm{p}<0.01$ ) and increased further at UT2 (FT-UT2, UT1-UT2; both p < 0.01). Differences in both COMvel-LAT and variability of COMvel-LAT were observed ( $\mathrm{F}_{2,20}=5.529$, $\mathrm{p}=0.012$ and $\mathrm{F}_{2,20}=34.453, \mathrm{p}<0.001$ respectively; Figure 4B). COMvel-LAT was on average higher on UT1 than FT ( $\mathrm{p}<0.01$ ), but was not different from FT at UT2 ( $\mathrm{p}>0.05$ ). variability of COMVEL-LAT was higher on UT1 in comparison to FT ( $\mathrm{p}<0.01$ ) and increased further at UT2 ( $\mathrm{p}<0.05$ ).

Significant differences in step width $\left(\mathrm{F}_{1.3,13.3}=16.312, \mathrm{p}=0.001\right.$; Figure 4 C$)$ and step width variability $\left(\mathrm{F}_{2,20}=29.805, \mathrm{p}<0.001\right)$ were observed. Step width was higher initially on uneven terrain at UT1 ( $\mathrm{p}<0.01$ ) but reduced ( $\mathrm{p}<0.01$ ) such that it was not different from FT at

UT2 ( $\mathrm{p}>0.05$ ). Step width variability was higher on UT1 in comparison to FT ( $\mathrm{p}<0.01$ ) and remained high (UT1-UT2 p > 0.05, FT-UT2 p < 0.01).

## Discussion

## Initial phase of walking on uneven terrain: Cautious and Variable

Average values for step length and width were comparable to previously reported values for flat and uneven terrain walking (Voloshina et al., 2013). The variability of these parameters was slightly lower in the present study; potentially a result of the differences in the treadmill surface. As anticipated, an immediate change in dynamics was observable as participants were first exposed to an uneven surface. Variability in COM excursion ranges, peak per-step velocities and foot placement in anterior and lateral directions was higher during the first 60 strides of walking on uneven terrain in comparison to FT. It is likely that some of this variability may be explained by trends inflating the spread of the data over the 60 steps, whilst participants became familiar with the surface, e.g. gradual increases in step length.

The changes in foot placement observed at UT1, i.e. increases in step width and decreases in step length, support the immediate adoption of a cautious and restrictive solution, and were as anticipated and consistent with previous literature (e.g. Hak et al., 2013; Voloshina et al., 2013, respectively). The hypothesized increases in average COM excursion and velocity on initial exposure to uneven terrain were observed only in the medial-lateral direction, but not the anterior-posterior direction. An orthogonal interplay between anterior-posterior versus medial-lateral control has similarly been observed in previous studies, which was suggested to illustrate the relative prioritization of progression in the direction of locomotion versus balance control (Bauby and Kuo, 2000; Wurdeman et al., 2012). While passive dynamics may effectively manage forward progression during level walking (Bauby and Kuo, 2000; Collins et al., 2005), lateral stability is believed to be under the control of higher centers (O'Connor and Kuo, 2009). In this novel task, a change in the medial-lateral direction accompanied by a lack of change in the anterior-posterior direction, evident despite the uneven support surface, may be a result of active anterior-posterior restriction as a means to avoid destabilization and to prioritize balance control in the early stages of exposure. The lack of change in anterior-posterior COM excursion and velocity may also be a secondary effect of the shorter step length, or merely due to the constraint of the fixed treadmill speed. The imposition of a fixed step length across conditions,
and repetition of the study on an overground uneven surface or self-paced uneven terrain treadmill could exclude the latter two of these hypotheses.

## Change in locomotor patterns on uneven terrain over time: Less restrictive but more refined

Changes in whole-body locomotor patterns were observed following a longer period of walking on the same surface in some, but not in all variables examined. Further, the changes were not consistent across anterior-posterior and medial-lateral directions. Against expectation, COM excursion range and its variability did not reduce at UT2. Anterior-posterior excursion range, in fact, increased at UT2, and the higher variability observed at UT1 was maintained, whereas medial-lateral excursion range did not change but its variability increased at UT2. Both of these findings, again, might indicate an initial self-imposed restriction to motion that was released with familiarity with the uneven terrain (Bernstein, 1967; Vereijken et al., 1992). These results are notable given that across the analysis period of UT1 the presence of any increasing or decreasing trend in COM excursion range would have inflated the standard deviation of the data.

In the anterior-posterior direction, increases in average step length and reductions in the variability of peak COM velocity and step length allude to an evolution of the dynamics in the direction of progression with time, consistent with reduction of conservative strategies and a more refined solution. These variables at UT2 remained significantly different to FT, however, indicating an enduring effect of the terrain. It remains possible that an increase in the duration of the trial, which permitted only approximately 11 minutes of exposure prior to analysis in the current study, or inclusion of additional bouts of walking on the uneven surface, would have led to greater refinement.

The elimination of the initial increase in step width and peak lateral COM velocity similarly suggest refinement of the solution in the medial-lateral direction. Conversely, a high variability of COM movement and high step width variability have been associated with poorer control of movement and greater fall risk in studies of level walking (e.g. (Brach et al., 2005)); therefore the observed increase in lateral variability over time might appear to support a degradation rather than a refinement in movement dynamics. However, an increase in lateral COM variability would arguably not present a risk to balance should an appropriate relationship between COM dynamics and base of support be maintained at each step. In order to further explore these unanticipated increases in variability, a post hoc analysis of the relationship
between COM and foot placement in the medial-lateral direction was performed. Based on the method of Wang et al. (Wang and Srinivasan, 2014) models to predict the lateral placement of the (dominant) swing foot based on medial-lateral COM state (excursion and velocity) during the preceding midstance were developed (for detailed methods refer to (Wang and Srinivasan, 2014), noting that in the present study whole-body COM was employed instead of pelvis, as Arvin et al. (2018)). Lateral step placement (analogous to step width in the present study) could be predicted by medial-lateral COM dynamics at the preceding midstance by the following equations, each based on 100 strides from each participant, with variables expressed as a deviation from the mean and coefficients averaged across the group:

FT: $\quad$ Foot placement $=1.84$ COM position +0.35 COM velocity
UT1: Foot placement $=1.59$ COM position +0.33 COM velocity
UT2: Foot placement $=1.73$ COM position +0.39 COM velocity
Greater excursion and velocity towards the swing foot was associated with a more lateral foot placement, and the relationship was maintained both on flat and uneven terrain. $\mathrm{R}^{2}$ values computed from correlations between predicted and measured lateral foot positions revealed that approximately $70 \%$ of the variance in step width could be predicted by medial-lateral position and velocity at midstance with respect to the stance foot (across the group FT: $72.6 \pm 8.1 \%$; UT1: $69.6 \pm 10.5 \%$; UT2: $73.0 \% \pm 5.9 \%$ ).

This post-hoc analysis indicates that the increased variabilities of individual variables that were observed in the medial-lateral direction are actually effectively controlled and managed by unimpaired individuals through the coupling between COM dynamics and foot placement. As such, the increase in variability of the medial-lateral variables may simply be due to a lack of threat once familiar with the constraints of the surface and their potential impact on movement. It is possible that the COM and step position variability in the medial-lateral direction is a direct consequence of the contours of the terrain that naturally perturb the person in the medial-lateral direction. One might speculate that it would be less profitable and more energetically costly to oppose these perturbations and attempt to restrict movement in this plane in the absence of a threat to stability. It is also possible that there is benefit to an increased variability in this direction as a form of exploratory behavior, enabling the surface to be actively probed from stride to stride (Vereijken et al., 1992).

In an alternate interpretation, the directional changes observed are consistent with optimization theories of motor control (Diedrichsen et al., 2010; Todorov and Jordan, 2002) and the minimum intervention principle (Scott, 2004; Todorov and Jordan, 2002), with the assertion that variability would be expected to be minimized only when it hinders the task goal; walking forwards on a moving belt. Alteration of the task context, by introducing a requirement to stabilize a container of liquid whilst walking for example, might reveal whether this lateral variability would be reduced should successful performance of the task demand it.

Although these results indicate a refinement of movement, it is unclear whether the adaptations may be associated with a greater walking economy. For example, whilst a reduction in step width and in step length variability over time might reduce metabolic cost (see (Donelan et al., 2001) and (Rock et al., 2018), respectively), the increase in step width variability could have the opposite effect (O'Connor et al., 2012). Direct measurement of energetics within the same experimental paradigm would provide further insight into this aspect of locomotor performance.

Despite differences in the terrain contour encountered from stride to stride, our findings suggest that individuals adapted their movement as they became familiar with the terrain. This implies that some understanding of the constraints of the surface and potential effects on the forces experienced during walking may be learned over time. Given the inherent periodicity of the pattern, such constraints might include the range of surface heights and the absence of abrupt changes in height. The manipulation of these factors, particularly in an unpredictable manner, may reduce the effectiveness of such refinements to movement and produce a different outcome. Similarly, the use of a treadmill will have introduced speed, step width and step length constraints associated with remaining safely in the center of the treadmill belt, potentially influencing the dynamics and variability of walking patterns on first exposure and after familiarization. Whether the same observations would be made without these constraints warrants testing. A further limitation to the study lies in the lack of inclusion of the first 60 strides of walking on the flat terrain (would be FT1). We performed this analysis under the presumption that treadmill walking was already a learned skill for these participants, and the flat and uneven terrain treadmills were similar, isolating the effect of the terrain. The results observed in the uneven terrain trial are unlikely to be a result of familiarization with walking on a moving belt given that participants had walked for over 12 minutes on flat terrain prior to
walking on uneven terrain. However, it is plausible that a similar trend in these measures would have been observed on the flat in addition to the uneven terrain (Owings and Grabiner, 2003; Taylor et al., 1996).

This study investigated the whole-body responses of unimpaired individuals for whom conservative strategies appropriate for this context appear to be readily available. The changes in the terrain were modest, permitting heel strike and foot-flat to be achieved regardless of the contour encountered at each step. The absence of adequate ankle range of motion or the inability to adjust compliance at the foot and ankle, as may be experienced by an orthosis or prosthesis user, would preclude this ability, leading to a greater disruption to walking. Similarly, the lack of ability to appropriately perceive relevant cues regarding changes in COM state could be severely disabling in this context, and necessitate conservative strategies to be continually employed in order to maintain balance. Further investigation of the strength of the relationship between COM dynamics and foot placement at different points in gait cycle, alongside the inclusion of anteriorposterior and vertical COM state variables may provide further insight into the time course of step-to-step adjustments given changes in terrain contour in unimpaired and pathological populations. Further, the exploration of rotational dynamics at joint and segmental level, both in concert and in isolation, will provide further insight into how these global solutions arise, and the implications of degradation, injury or absence of joints for the ability of an individual to readily negotiate non-level environments.

## Conclusions

Our results indicate that the whole-body locomotor dynamics of unimpaired individuals are affected by modest changes in terrain, and that movement solutions can evolve over time with longer exposure to the surface, despite changes in the interactions experienced from stride to stride. In the direction of walking, dynamics appeared to become more refined with time. In contrast, perpendicular to the direction of walking, the changes over time were consistent with a release of degrees of freedom, but one that is effectively managed when observing the system as a whole. Future work will explore the means by which these immediate and longer-term solutions are brought about, and the extent to which success of the task depends on controllable degrees of freedom, with implications for individuals with lower limb pathology or amputation.

## List of symbols and abbreviations

| AP | Anterior-posterior |
| :--- | :--- |
| $\sim$ ANT | In the anterior direction |
| COM | Center of mass |
| COMEXC | Whole-body center of mass excursion range |
| COMVEL | Whole-body center of mass peak velocity |
| FT | Flat terrain |
| ML | Medial-lateral |
| $\sim$ LAT | In the lateral direction |
| UT | Uneven terrain |
| UT1 | Start of uneven terrain trial |
| UT2 | End of uneven terrain trial |

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## Competing interests

No competing interests declared.

## Author contributions

JK acquired, analyzed and interpreted the data, and drafted the manuscript. JK and NS were responsible for the conception and design of the work. JS contributed to the experimental design, acquired and processed the data and revised the manuscript for intellectual content. MM contributed to the interpretation of data and revised the manuscript for intellectual content. KT contributed to experimental design and analysis, and revised the manuscript for intellectual content. NS contributed to the conception and design of the study, and the interpretation of the data, and revised the manuscript for intellectual content. All authors read and approved the final manuscript.

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## Data availability

The dataset analyzed during the current study are available from the corresponding author on reasonable request.

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Table 1. Mean (standard deviation) of midstance foot angle range and variability across 60 strides on a standard flat treadmill (FT), and at the beginning (UT1) and end (UT2) of a 12minute trial on an uneven terrain treadmill.

| Plane |  | FT | UT1 | UT2 |
| :--- | :--- | :--- | :--- | :--- |
| Sagittal | Range $\left({ }^{\circ}\right)$ | $1.5(0.1)$ | $10.5(0.2)^{*}$ | $10.6(0.5)^{*}$ |
|  | Standard deviation $\left({ }^{\circ}\right)$ | $0.3(0.6)$ | $3.0(1.0)^{*}$ | $3.0(1.4)^{*}$ |
| Coronal | Range $\left({ }^{\circ}\right)$ | $3.6(0.3)$ | $12.4(0.3)^{*}$ | $12.5(0.6)^{*}$ |
|  | Standard deviation $\left({ }^{\circ}\right)$ | $0.8(1.0)$ | $2.9(2.6)^{*}$ | $2.9(2.5)^{*}$ |

*significantly different from FT (p < 0.05). There were no differences observed between UT1 and UT2.

## Figures



Figure 1. Uneven terrain treadmill. The uneven terrain surface is comprised of manuallyshaped wooden slats affixed to a standard treadmill belt perpendicular to the direction of travel. The repeating pattern has four levels, in increments of $7 \mathrm{~mm}, 7 \mathrm{~mm}$ and 8 mm from the lowest level (maximum depth of approximately 2.2 cm ); selected as sufficiently shallow to enable a heel-toe gait to be maintained. The contours of the pattern were designed such that, unless deliberate targeting is attempted, each step on the surface should result in a slightly different interaction. The pattern is reflected and offset such that both feet should have equal probability of encountering the same contours.


Figure 2. Variables. Anterior-posterior (AP) and Medial-lateral (ML) center of mass (COM) and step placement.


Figure 3. Center of mass (COM) and step dynamics in the anterior-posterior direction. Average (mean; left) and variability (standard deviation; right) across 60 strides on flat terrain (FT) and uneven terrain, at the beginning (UT1) and end (UT2) of a 12-min walking trial. Circles represent individual subject results; crosses represent mean value. (A) per-step COM excursion range, (B) peak per-step anterior COM velocity, (C) step length. $\mathrm{N}=11$, $*$ p $<0.05$, in post-hoc Tukey's HSD/Wilcoxon (for Average Peak Anterior COM Velocity only) signed rank tests.


Figure 4. Center of mass (COM) and step dynamics in the medial-lateral direction. Average (mean; left) and variability (standard deviation; right) across 60 strides on flat terrain (FT) and uneven terrain, at the beginning (UT1) and end (UT2) of a $12-\mathrm{min}$ walking trial. Circles represent individual subject results; crosses represent mean value. (A) per-step COM excursion range, (B) peak per-step lateral COM velocity, (C) step width. $\mathrm{N}=11$, , p < 0.05 , in post-hoc Tukey's HSD tests.

## FULL BODY MODEL - DESCRIPTION

Table S1. Model Fundamentals

| Design | In house developed full body model and location protocol. |
| :--- | :--- |
| Degrees of freedom | All joints/segments : 6 |
| Optimisation | Segment optimisation - Software generic. <br> See Visual 3D documentation at <br> http://www.c-motion.com/v3dwiki/index.php? title=Six_Degrees_of Freedom and ${ }^{1}$ |
| Kinetic calculations | Mass, moments of inertia and center of gravity calculated according to ${ }^{2}$ (see Visual 3D documentation at http://c- <br> motion.com/v3dwiki/index.php/Segment_Geometry |

Table S2. Landmarks

| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| $\wedge$ ASI | Superficial on skin surface such that marker body is anterior to prominent anterior edge of iliac crest. | Palpation | Yes | Yes | Marker |
| $\wedge$ PSI | Superficial to palpable prominence at posterior edge of iliac crest. | Palpation | No | Yes | Marker |
| $\wedge$ ^ASI2 | Superficial and lateral to proximal border of iliac crest. | Palpation | No | Yes | Marker |
| ${ }^{\wedge}$ VPSI | PSI projected by half marker radius perpendicular to contralateral PSI in plane connecting PSIs and mid point between ASIs. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VASI | ASI projected by half marker radius perpendicular to contralateral ASI in plane connecting ASIs and mid point between PSIs. | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HJC}$ | Hip joint centre - at the following distances from mid-point between VASI markers (Pelvis origin) in pelvis coordinate system (see Pelvis): <br> $\mathrm{AP}($ in mm$)=-0.24 \mathrm{PD}-9.9$ <br> $\mathrm{ML}($ in mm$)=0.28 \mathrm{PD}+0.16 \mathrm{PW}+7.9$ <br> Axial $($ in mm $)=-0.16 \mathrm{PW}-0.04 \mathrm{LL}-7.1$ <br> Where PD = Pelvic depth: the distance between the mid points of VASIs and VPSIs <br> PW = Pelvic width : distance between left and right VASIs <br> LL $=$ Leg Length : distance between the ASI and VANM via the VKNM ${ }^{3}$ | Calculation | Yes | No | Derived |


| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge}$ TRO | Lateral and superficial to the centre of the palpated prominence of the greater trochanter when standing in calibration posture. | Palpation | No | Yes | Marker |
| $\wedge$ TH1 | Anteriorly on thigh, approximately $1 / 3$ distance between hip and knee. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge} \mathrm{TH} 2$ | Anteriorly on thigh, 50 mm (approx.) above the patella when relaxed in standing. | Visualisation | No | Yes | Marker |
| ^TH3 | Laterally on thigh, approximately mid distance between hip and knee | Visualisation | No | Yes | Marker |
| $\wedge$ TH4 | Lateral on thigh, between TH3 and TRO | Visualisation | No | Yes | Marker |
| ${ }^{\wedge} \mathrm{KNL}$ | At the bony prominence of the lateral femoral condyle, to form the lateral end of a 'knee axis' with ^KNM. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{KNM}$ | At the bony prominence of the medial femoral condyle, to form the medial end of a 'knee axis' with ^${ }^{\wedge}$ KNL. | Palpation | Yes | No | Marker |
| ${ }^{\wedge}$ VKNL | KNL projected by half marker radius in direction of KNM. | Calculation | Yes | No | Derived |
| $\wedge$ VKNM | KNM projected by half marker radius in direction of KNL. | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{KJC}$ | Mid point between KNL and KNM. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ SHA1-4 | Set of four markers placed anteriorly and posteriorly on lower $1 / 3$ of the shank positioned to avoid excessive rotation due to individual tendon/muscle protrusion on dorsi/plantar flexion. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge}$ ANL | At most lateral point on lateral malleolus, to form the lateral end of the 'ankle' axis with $\wedge$ ANM. | Palpation | Yes | No | Marker |
| $\wedge$ ANM | At most medial point on medial malleolus, to form the medial end of the 'ankle' axis with $\wedge$ ANL. | Palpation | Yes | No | Marker* |
| ${ }^{\wedge}$ VANL | ANL projected by half marker radius in direction of ANM. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VANM | ANM projected by half marker radius in direction of ANL. | Calculation | Yes | No | Derived |
| $\wedge$ AJC | Mid point between ANL and ANM |  |  |  |  |
| ^TOE | At a point approximating position of second metatarsal head on dorsum of shoe | Palpation /Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{MT} 1$ | On dorsum of shoe at a point approximating position of first metatarsal head. | Palpation /Visualisation | Kinetic only | Yes | Marker |
| ${ }^{\wedge} \mathrm{MT} 5$ | On dorsum of shoe at a point approximating position of fifth metatarsal head. | Palpation /Visualisation | Kinetic only | Yes | Marker |
| ${ }^{\wedge} \mathrm{FT} 3$ | On dorsum of shoe proximal to MT1 and MT5. | Palpation /Visualisation | No | Yes | Marker |


| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge} \mathrm{HEE}$ | On heel counter, approximately 15 mm from ground, centrally when viewing from a posterior position along the long axis of the shoe to form the longitudinal axis of the foot with TOE | Measurement /Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge}$ TOEvert | Projection of TOE onto laboratory floor. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ HEEvert | Projection of HEE onto laboratory floor. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ HEElat | Projection of HEEvert laterally in pelvis coordinate system. | Calculation | Yes | No | Derived |
| STRN | Anterior and superficial to sternal notch | Palpation | Yes | Yes | Marker |
| XYPH | Superficial to xyphoid process | Palpation | Yes | Yes | Marker |
| C7 | Superficial to seventh cervical vertebra | Palpation | Yes | Yes | Marker |
| LUM | Lumbar region, superficial to the spine at point of maximum curvature. | Palpation | Yes | Yes | Marker |
| LowerTorso | Mid point between XYPH and LUM | Palpation | Yes | No | Marker |
| UpperTorso | Mid point between STRN and C7 | Palpation | Yes | No | Marker |
| ${ }^{\wedge}$ SHA | Anterior to the approximate shoulder joint centre. | Palpation/ Visualisation | Yes | Yes | Marker |
| $\wedge$ ACR | Vertically above the acromium process | Palpation | Yes | No | Marker * |
| ${ }^{\wedge} \mathrm{SJC}$ | Projection of SHA onto the plane made by R \& LACR and the vertical projection of RACR. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ UPA | On the posterior upper arm approximately half way between the shoulder and elbow. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge}$ ELL | Superficial to the lateral condyle, placed with the arm hanging to the side of the body | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge}$ ELM | Approximately superficial to the medial condyle, placed with the arm hanging to the side of the body to form an axis through the elbow with ELL | Palpation | Yes | No | Marker <br> * |
| ${ }^{\wedge}$ VELL | ELL projected by half marker radius in direction of ELM | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VELM | ELM projected by half marker radius in direction of ELL | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ EJC | Mid point between ELL and ELM | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HA} 1$ | Between $1^{\text {st }}$ and $2^{\text {nd }}$ metacarpals, approximately 15 mm from the metacarpal heads. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HA} 2$ | On the radial process of the wrist, to form a 'wrist axis' through the joint with HA3. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HA} 3$ | On the ulnar process of the wrist, to form a 'wrist axis' through the joint with HA2. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge}$ VHA2 | HA2 projected by half marker radius in direction of HA3 | Calculation | Yes | No | Derived |


| Landmark ID (^bilateral/side) | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge} \mathrm{VHA} 3$ | HA3 projected by half marker radius in direction of HA2 | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{FIN}$ | HA1 projected distally $0.5^{*}$ distance between HA1 and midpoint of HA2 and HA3, along the line formed by HA1 and then midpoint of HA2 and HA3 | Calculation | Yes | No | Derived |
| $\wedge$ ^FHD | On band approximately 2 cm above brow line, vertically above corner of eye | Visualisation | Yes | Yes | Marker |
| ^BHD | On band approximately 2 cm laterally of bony protrusion on back of head | Palpation/ Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HEC}$ | Mid point of line between FHD and BHD | Calculation | Yes | No | Derived |
| LFHD _proj | LFHD projected backwards in global coordinate system by 0.05 m | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HEP}$ | HEC projected (upwards) onto plane defined by RFHD, LFHD and LFHD proj | Calculation | Yes | No | Derived |

* Marker removed following static calibration trial

Table S3. Segment definitions

| $\begin{aligned} & \text { Segment } \\ & \text { (^bilateral/ } \\ & \text { side) } \end{aligned}$ | Landmarks (derived landmarks in parentheses) | Origin | Axes |  |  | Geometry* <br> Joint radii | Tracking markers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Flex/ext | Add/abd | Axial |  |  |
| Pelvis (V3D <br> Composite ${ }^{\text {a }}$ ) | LASI, RASI, LPSI, RPSI, LAS2, RAS2, (LVASI), (RVASI), (LVPSI), (RVPSI) | Midpoint between LVASI and RVASI markers | Parallel to line from origin to RVASI | Orthogonal to the flex/ext and axial axes. | Perpendicular to the plane defined by LVASI, RVASI \& the midpoint between LVPSI and RVPSI | See ${ }^{\text {a }}$ | LASI, RASI, LPSI, RPSI, LAS2, RAS2, VSAC |
| ${ }^{\wedge}$ Thigh | (VKNL), (VKNM), TRO, TH1, TH2, TH3, KNL (HJC) | HJC | Perpendicular to axial axis in plane defined by HJC, VKNL and VKNM | Orthogonal to axial and flex/ext axes | Line joining HJC and midpoint between VKNL and VKNM | Proximal: half distance between RTRO and LTRO | $\begin{gathered} \text { TRO, TH1-4, } \\ \text { KNL }^{\mathrm{b}} \end{gathered}$ |
| ${ }^{\wedge}$ Shank | (KJC), (VANL), (VANM), ANL, SK1-4 | KJC | Perpendicular to axial axis in plane defined by KJC, VANL and VANM | Orthogonal to Axial and Flex/Ext axes | Line joining KJC and midpoint between VANL and VANM | Proximal: half distance between VANL and VANM | $\begin{gathered} \text { SK1-4, KNL, } \\ \text { ANL }^{\text {b }} \end{gathered}$ |
| ${ }^{\wedge}$ Foot | $\begin{gathered} \text { (AJC), (VANL), } \\ \text { TOE, LHL, } \\ \text { HEE, MT5 } \end{gathered}$ | AJC | Perpendicular to axial axis in plane defined by AJC, VANL and TOE | Orthogonal to Axial and Flex/Ext axes | Line joining AJC and TOE | Proximal : distance between AJC and VANL, Distal : half distance between MT1 and MT5 | TOE, HEE, MT1, MT5, FT3 |
| ${ }^{\wedge}$ KMAT Foot | (HEEvert), (TOEvert), (HEElat), TOE, LHL, HEE, MT5 | HEEvert | Perpendicular to axial axis in plane defined by HEEvert, TOEvert and HEElat | Line joining HEEvert and TOEvert | Orthogonal to Add/Abd and Flex/Ext axes | NA | TOE, HEE, MT1, MT5, FT3 |


| $\begin{aligned} & \text { Segment } \\ & \text { (^bilateral/ } \\ & \text { side) } \end{aligned}$ | Landmarks (derived landmarks in parentheses) | Origin | Axes |  |  | Geometry* <br> Joint radii | Tracking markers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Flex/ext | Add/abd | Axial |  |  |
| Thorax | (UpperTorso), (LowerTorso), STRN, XYPH, C7, LUM. | Upper <br> Torso | Perpendicular to axial axis, orthogonal to plane defined by UpperTorso, LowerTorso and STRN. | Orthogonal to Axial and Flex/Ext axes | Line joining UpperTorso and LowerTorso | Proximal : half distance between RSJC and LSJC <br> Distal : half distance between RASI and LASI | $\begin{gathered} \text { STRN, } \\ \text { XYPH, C7, } \\ \text { LUM } \end{gathered}$ |
| ^ Upper Arm | $\begin{gathered} \text { (SJC), UPA, } \\ \text { (VELL), } \\ \text { (VELM), SHA, } \\ \text { ELL } \end{gathered}$ | SJC | Perpendicular to axial axis in plane defined by SJC, VELL and VELM | Orthogonal to Axial and Flex/Ext axes | Line joining SJC to mid point between VELL and VELM | Proximal : distance between SJC and ACR | SHA, UPA, ELL |
| ${ }^{\wedge}$ Forearm | $\begin{gathered} \text { (EJC), (VHA2), } \\ \text { (VHA3), ELL, } \\ \text { HA2, HA3 } \end{gathered}$ | EJC | Perpendicular to axial axis in plane defined by EJC, VHA2 and VHA3 | Orthogonal to Axial and Flex/Ext axes | Line joining EJC to mid point between VHA2 and VHA3 | Proximal : distance between VELL and VELM | $\begin{gathered} \text { ELL, HA2, } \\ \text { HA3 } \end{gathered}$ |
| Hand | $\begin{gathered} \text { (FIN), HA1, } \\ \text { HA2, HA3, } \\ \text { (VHA2), } \\ \text { (VHA3) } \end{gathered}$ | Midpoint between VHA2 and VHA3 | Perpendicular to axial axis in plane defined by FIN, VHA2 and VHA3 | Orthogonal to Axial and Flex/Ext axes | Line joining FIN and midpoint between VHA2 and VHA3 | Distal : half distance between VHA2 and VHA3 | $\begin{gathered} \text { HA1, HA2, } \\ \text { HA3 } \end{gathered}$ |
| Head | (RHE),(LHE), <br> (Upper Torso), <br> LFHD, RFHD, <br> LBHD, RBHD | Mid point between RHE and LHE | Perpendicular to axial axis in plane defined by RHE, LHE and Upper Torso | Orthogonal to Axial and Flex/Ext axes | Line joining mid point between RHE and LHE and Upper Torso | Proximal : Half distance between LFHD and LBHD minus 1 marker diameter. Depth : half distance between LFHD and LBHD minus 1 marker diameter | LFHD, <br> RFHD, <br> LBHD, <br> RBHD |

${ }^{\text {a }}$ See http://www.c-motion.com/v3dwiki/index.php?title=V3D Composite Pelvis
${ }^{b}$ Data from repeatedly obscured markers excluded. Segments tracked with at least 3 non-collinear markers including at least 1 anterior and 1 posterior placed marker.

Table S4. Joint definitions / rotation sequences

| Joint / Segment angle name <br> (*bilateral) | Segment $^{\mathbf{b}}$ | Reference segment $^{\mathbf{b}}$ | Cardan sequence | Positive direction |
| :---: | :---: | :---: | :---: | :---: |
| Pelvis | Pelvis | Laboratory | Flex/ext - add/abd - int/ext rotation | Tilt - anterior <br> Obliquity - right down <br> Twist - right forwards |
| Hip* | Thigh | Pelvis | Flex/ext - add/abd - int/ext rotation | Flexion <br> Adduction <br> Internal rotation |
| Knee* | Shank | Thigh | Flex/ext - add/abd - int/ext rotation | Flexion <br> Adduction <br> Internal rotation |
| Ankle* | Foot | Shank | Flex/ext-add/abd-inv/ev rotation | Dorsiflexion <br> Adduction <br> Inversion |
| Virtual Ankle* | Virtual Foot | Virtual Shank | Flex/ext-inv/ev-add/abd | Dorsiflexion <br> Inversion <br> Adduction |

${ }^{\text {a }}$ Virtual segments are used for joint kinematics only.
${ }^{\mathrm{b}}$ Angles are calculated within the co-ordinate system of the reference segment.

## Table S5. System

| Capture system / software | Motion Analysis Corporation ${ }^{\text {a }}: 17$-camera Raptor/ Cortex version $6^{\text {a }}$ |
| :--- | :--- |
| Medium | Passive retro-reflective markers $: 12.7 \mathrm{~mm}$ with thin fabric base |
| Sampling frequency | 100 Hz |

Table S6. Processing

|  | Software |  |
| :--- | :---: | :--- |
| Eventing | Visual 3D $^{\mathrm{b}}$ | Kinematic algorithm (velocity-based, from ${ }^{4}$ ) |
| Filtering | Visual 3D $^{\mathrm{b}}$ | 7Hz-12Hz 4 4 ${ }^{\text {th }}$ order Butterworth, by marker ${ }^{5}$ |
| Interpolation | Cortex $^{\mathrm{a}}$ | Cubic spline / software-based virtual join ${ }^{\mathrm{a}}$ |

${ }^{a}$ Motion Analysis Corporation, Santa Rosa, CA, USA
${ }^{\mathrm{b}}$ C-Motion, Germantown, MD, USA
${ }^{\text {c }}$ Mathworks, Natick, MA, USA

## References

${ }^{1}$ Spoor CW. Rigid body motion calculated from spatial co-ordinates of markers. J. Biomech 1980; 13: 391-393.
${ }^{2}$ Hanavan Jr, EP. A mathematical model of the human body (No. AFIT-GA-PHYS-64-3). Air Force Aerospace Medical Research Lab Wright-Patterson Afb Oh, 1964.
${ }^{3}$ Harrington ME, Zavatsky AB, Lawson SE, Yuan Z, Theologis TN. Prediction of the hip joint centre in adults, children, and patients with cerebral palsy based on magnetic resonance imaging. J Biomech. 2007;40(3):595-602.
${ }^{4}$ Zeni Jr, JA., Richards, JG, \& Higginson, JS. Two simple methods for determining gait events during treadmill and overground walking using kinematic data. Gait Posture 2008, 27(4), 710-714.
${ }^{5}$ Giakas, G. Power spectrum analysis and filtering. Innovative Analyses of Human Movement, Champaign, IL: Human Kinetics, 2004.

## FULL BODY MODEL - DESCRIPTION

Table S1. Model Fundamentals

| Design | In house developed full body model and location protocol. |
| :--- | :--- |
| Degrees of freedom | All joints/segments : 6 |
| Optimisation | Segment optimisation - Software generic. <br> See Visual 3D documentation at <br> http://www.c-motion.com/v3dwiki/index.php? title=Six_Degrees_of Freedom and ${ }^{1}$ |
| Kinetic calculations | Mass, moments of inertia and center of gravity calculated according to ${ }^{2}$ (see Visual 3D documentation at http://c- <br> motion.com/v3dwiki/index.php/Segment_Geometry |

Table S2. Landmarks

| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| $\wedge$ ASI | Superficial on skin surface such that marker body is anterior to prominent anterior edge of iliac crest. | Palpation | Yes | Yes | Marker |
| $\wedge$ PSI | Superficial to palpable prominence at posterior edge of iliac crest. | Palpation | No | Yes | Marker |
| $\wedge$ ^ASI2 | Superficial and lateral to proximal border of iliac crest. | Palpation | No | Yes | Marker |
| ${ }^{\wedge}$ VPSI | PSI projected by half marker radius perpendicular to contralateral PSI in plane connecting PSIs and mid point between ASIs. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VASI | ASI projected by half marker radius perpendicular to contralateral ASI in plane connecting ASIs and mid point between PSIs. | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HJC}$ | Hip joint centre - at the following distances from mid-point between VASI markers (Pelvis origin) in pelvis coordinate system (see Pelvis): <br> $\mathrm{AP}($ in mm$)=-0.24 \mathrm{PD}-9.9$ <br> $\mathrm{ML}($ in mm$)=0.28 \mathrm{PD}+0.16 \mathrm{PW}+7.9$ <br> Axial $($ in mm $)=-0.16 \mathrm{PW}-0.04 \mathrm{LL}-7.1$ <br> Where PD = Pelvic depth: the distance between the mid points of VASIs and VPSIs <br> PW = Pelvic width : distance between left and right VASIs <br> LL $=$ Leg Length : distance between the ASI and VANM via the VKNM ${ }^{3}$ | Calculation | Yes | No | Derived |


| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge}$ TRO | Lateral and superficial to the centre of the palpated prominence of the greater trochanter when standing in calibration posture. | Palpation | No | Yes | Marker |
| $\wedge$ TH1 | Anteriorly on thigh, approximately $1 / 3$ distance between hip and knee. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge} \mathrm{TH} 2$ | Anteriorly on thigh, 50 mm (approx.) above the patella when relaxed in standing. | Visualisation | No | Yes | Marker |
| ^TH3 | Laterally on thigh, approximately mid distance between hip and knee | Visualisation | No | Yes | Marker |
| $\wedge$ TH4 | Lateral on thigh, between TH3 and TRO | Visualisation | No | Yes | Marker |
| ${ }^{\wedge} \mathrm{KNL}$ | At the bony prominence of the lateral femoral condyle, to form the lateral end of a 'knee axis' with ^KNM. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{KNM}$ | At the bony prominence of the medial femoral condyle, to form the medial end of a 'knee axis' with ^${ }^{\wedge}$ KNL. | Palpation | Yes | No | Marker |
| ${ }^{\wedge}$ VKNL | KNL projected by half marker radius in direction of KNM. | Calculation | Yes | No | Derived |
| $\wedge$ VKNM | KNM projected by half marker radius in direction of KNL. | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{KJC}$ | Mid point between KNL and KNM. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ SHA1-4 | Set of four markers placed anteriorly and posteriorly on lower $1 / 3$ of the shank positioned to avoid excessive rotation due to individual tendon/muscle protrusion on dorsi/plantar flexion. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge}$ ANL | At most lateral point on lateral malleolus, to form the lateral end of the 'ankle' axis with $\wedge$ ANM. | Palpation | Yes | No | Marker |
| $\wedge$ ANM | At most medial point on medial malleolus, to form the medial end of the 'ankle' axis with $\wedge$ ANL. | Palpation | Yes | No | Marker* |
| ${ }^{\wedge}$ VANL | ANL projected by half marker radius in direction of ANM. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VANM | ANM projected by half marker radius in direction of ANL. | Calculation | Yes | No | Derived |
| $\wedge$ AJC | Mid point between ANL and ANM |  |  |  |  |
| ^TOE | At a point approximating position of second metatarsal head on dorsum of shoe | Palpation /Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{MT} 1$ | On dorsum of shoe at a point approximating position of first metatarsal head. | Palpation /Visualisation | Kinetic only | Yes | Marker |
| ${ }^{\wedge} \mathrm{MT} 5$ | On dorsum of shoe at a point approximating position of fifth metatarsal head. | Palpation /Visualisation | Kinetic only | Yes | Marker |
| ${ }^{\wedge} \mathrm{FT} 3$ | On dorsum of shoe proximal to MT1 and MT5. | Palpation /Visualisation | No | Yes | Marker |


| $\begin{gathered} \text { Landmark ID } \\ \text { (^bilateral/side) } \end{gathered}$ | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge} \mathrm{HEE}$ | On heel counter, approximately 15 mm from ground, centrally when viewing from a posterior position along the long axis of the shoe to form the longitudinal axis of the foot with TOE | Measurement /Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge}$ TOEvert | Projection of TOE onto laboratory floor. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ HEEvert | Projection of HEE onto laboratory floor. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ HEElat | Projection of HEEvert laterally in pelvis coordinate system. | Calculation | Yes | No | Derived |
| STRN | Anterior and superficial to sternal notch | Palpation | Yes | Yes | Marker |
| XYPH | Superficial to xyphoid process | Palpation | Yes | Yes | Marker |
| C7 | Superficial to seventh cervical vertebra | Palpation | Yes | Yes | Marker |
| LUM | Lumbar region, superficial to the spine at point of maximum curvature. | Palpation | Yes | Yes | Marker |
| LowerTorso | Mid point between XYPH and LUM | Palpation | Yes | No | Marker |
| UpperTorso | Mid point between STRN and C7 | Palpation | Yes | No | Marker |
| ${ }^{\wedge}$ SHA | Anterior to the approximate shoulder joint centre. | Palpation/ Visualisation | Yes | Yes | Marker |
| $\wedge$ ACR | Vertically above the acromium process | Palpation | Yes | No | Marker * |
| ${ }^{\wedge} \mathrm{SJC}$ | Projection of SHA onto the plane made by R \& LACR and the vertical projection of RACR. | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ UPA | On the posterior upper arm approximately half way between the shoulder and elbow. | Visualisation | No | Yes | Marker |
| ${ }^{\wedge}$ ELL | Superficial to the lateral condyle, placed with the arm hanging to the side of the body | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge}$ ELM | Approximately superficial to the medial condyle, placed with the arm hanging to the side of the body to form an axis through the elbow with ELL | Palpation | Yes | No | Marker <br> * |
| ${ }^{\wedge}$ VELL | ELL projected by half marker radius in direction of ELM | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ VELM | ELM projected by half marker radius in direction of ELL | Calculation | Yes | No | Derived |
| ${ }^{\wedge}$ EJC | Mid point between ELL and ELM | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HA} 1$ | Between $1^{\text {st }}$ and $2^{\text {nd }}$ metacarpals, approximately 15 mm from the metacarpal heads. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HA} 2$ | On the radial process of the wrist, to form a 'wrist axis' through the joint with HA3. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HA} 3$ | On the ulnar process of the wrist, to form a 'wrist axis' through the joint with HA2. | Palpation | Yes | Yes | Marker |
| ${ }^{\wedge}$ VHA2 | HA2 projected by half marker radius in direction of HA3 | Calculation | Yes | No | Derived |


| Landmark ID (^bilateral/side) | Location | Location method | Function |  | Type |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Definition | Tracking |  |
| ${ }^{\wedge} \mathrm{VHA} 3$ | HA3 projected by half marker radius in direction of HA2 | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{FIN}$ | HA1 projected distally $0.5^{*}$ distance between HA1 and midpoint of HA2 and HA3, along the line formed by HA1 and then midpoint of HA2 and HA3 | Calculation | Yes | No | Derived |
| $\wedge$ ^FHD | On band approximately 2 cm above brow line, vertically above corner of eye | Visualisation | Yes | Yes | Marker |
| ^BHD | On band approximately 2 cm laterally of bony protrusion on back of head | Palpation/ Visualisation | Yes | Yes | Marker |
| ${ }^{\wedge} \mathrm{HEC}$ | Mid point of line between FHD and BHD | Calculation | Yes | No | Derived |
| LFHD _proj | LFHD projected backwards in global coordinate system by 0.05 m | Calculation | Yes | No | Derived |
| ${ }^{\wedge} \mathrm{HEP}$ | HEC projected (upwards) onto plane defined by RFHD, LFHD and LFHD proj | Calculation | Yes | No | Derived |

* Marker removed following static calibration trial

Table S3. Segment definitions

| $\begin{aligned} & \text { Segment } \\ & \text { (^bilateral/ } \\ & \text { side) } \end{aligned}$ | Landmarks (derived landmarks in parentheses) | Origin | Axes |  |  | Geometry* <br> Joint radii | Tracking markers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Flex/ext | Add/abd | Axial |  |  |
| Pelvis (V3D <br> Composite ${ }^{\text {a }}$ ) | LASI, RASI, LPSI, RPSI, LAS2, RAS2, (LVASI), (RVASI), (LVPSI), (RVPSI) | Midpoint between LVASI and RVASI markers | Parallel to line from origin to RVASI | Orthogonal to the flex/ext and axial axes. | Perpendicular to the plane defined by LVASI, RVASI \& the midpoint between LVPSI and RVPSI | See ${ }^{\text {a }}$ | LASI, RASI, LPSI, RPSI, LAS2, RAS2, VSAC |
| ${ }^{\wedge}$ Thigh | (VKNL), (VKNM), TRO, TH1, TH2, TH3, KNL (HJC) | HJC | Perpendicular to axial axis in plane defined by HJC, VKNL and VKNM | Orthogonal to axial and flex/ext axes | Line joining HJC and midpoint between VKNL and VKNM | Proximal: half distance between RTRO and LTRO | $\begin{gathered} \text { TRO, TH1-4, } \\ \text { KNL }^{\mathrm{b}} \end{gathered}$ |
| ${ }^{\wedge}$ Shank | (KJC), (VANL), (VANM), ANL, SK1-4 | KJC | Perpendicular to axial axis in plane defined by KJC, VANL and VANM | Orthogonal to Axial and Flex/Ext axes | Line joining KJC and midpoint between VANL and VANM | Proximal: half distance between VANL and VANM | $\begin{gathered} \text { SK1-4, KNL, } \\ \text { ANL }^{\text {b }} \end{gathered}$ |
| ${ }^{\wedge}$ Foot | $\begin{gathered} \text { (AJC), (VANL), } \\ \text { TOE, LHL, } \\ \text { HEE, MT5 } \end{gathered}$ | AJC | Perpendicular to axial axis in plane defined by AJC, VANL and TOE | Orthogonal to Axial and Flex/Ext axes | Line joining AJC and TOE | Proximal : distance between AJC and VANL, Distal : half distance between MT1 and MT5 | TOE, HEE, MT1, MT5, FT3 |
| ${ }^{\wedge}$ KMAT Foot | (HEEvert), (TOEvert), (HEElat), TOE, LHL, HEE, MT5 | HEEvert | Perpendicular to axial axis in plane defined by HEEvert, TOEvert and HEElat | Line joining HEEvert and TOEvert | Orthogonal to Add/Abd and Flex/Ext axes | NA | TOE, HEE, MT1, MT5, FT3 |


| $\begin{aligned} & \text { Segment } \\ & \text { (^bilateral/ } \\ & \text { side) } \end{aligned}$ | Landmarks (derived landmarks in parentheses) | Origin | Axes |  |  | Geometry* <br> Joint radii | Tracking markers |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Flex/ext | Add/abd | Axial |  |  |
| Thorax | (UpperTorso), (LowerTorso), STRN, XYPH, C7, LUM. | Upper <br> Torso | Perpendicular to axial axis, orthogonal to plane defined by UpperTorso, LowerTorso and STRN. | Orthogonal to Axial and Flex/Ext axes | Line joining UpperTorso and LowerTorso | Proximal : half distance between RSJC and LSJC <br> Distal : half distance between RASI and LASI | $\begin{gathered} \text { STRN, } \\ \text { XYPH, C7, } \\ \text { LUM } \end{gathered}$ |
| ^ Upper Arm | $\begin{gathered} \text { (SJC), UPA, } \\ \text { (VELL), } \\ \text { (VELM), SHA, } \\ \text { ELL } \end{gathered}$ | SJC | Perpendicular to axial axis in plane defined by SJC, VELL and VELM | Orthogonal to Axial and Flex/Ext axes | Line joining SJC to mid point between VELL and VELM | Proximal : distance between SJC and ACR | SHA, UPA, ELL |
| ${ }^{\wedge}$ Forearm | $\begin{gathered} \text { (EJC), (VHA2), } \\ \text { (VHA3), ELL, } \\ \text { HA2, HA3 } \end{gathered}$ | EJC | Perpendicular to axial axis in plane defined by EJC, VHA2 and VHA3 | Orthogonal to Axial and Flex/Ext axes | Line joining EJC to mid point between VHA2 and VHA3 | Proximal : distance between VELL and VELM | $\begin{gathered} \text { ELL, HA2, } \\ \text { HA3 } \end{gathered}$ |
| Hand | $\begin{gathered} \text { (FIN), HA1, } \\ \text { HA2, HA3, } \\ \text { (VHA2), } \\ \text { (VHA3) } \end{gathered}$ | Midpoint between VHA2 and VHA3 | Perpendicular to axial axis in plane defined by FIN, VHA2 and VHA3 | Orthogonal to Axial and Flex/Ext axes | Line joining FIN and midpoint between VHA2 and VHA3 | Distal : half distance between VHA2 and VHA3 | $\begin{gathered} \text { HA1, HA2, } \\ \text { HA3 } \end{gathered}$ |
| Head | (RHE),(LHE), <br> (Upper Torso), <br> LFHD, RFHD, <br> LBHD, RBHD | Mid point between RHE and LHE | Perpendicular to axial axis in plane defined by RHE, LHE and Upper Torso | Orthogonal to Axial and Flex/Ext axes | Line joining mid point between RHE and LHE and Upper Torso | Proximal : Half distance between LFHD and LBHD minus 1 marker diameter. Depth : half distance between LFHD and LBHD minus 1 marker diameter | LFHD, <br> RFHD, <br> LBHD, <br> RBHD |

${ }^{\text {a }}$ See http://www.c-motion.com/v3dwiki/index.php?title=V3D Composite Pelvis
${ }^{b}$ Data from repeatedly obscured markers excluded. Segments tracked with at least 3 non-collinear markers including at least 1 anterior and 1 posterior placed marker.

Table S4. Joint definitions / rotation sequences

| Joint / Segment angle name <br> (*bilateral) | Segment $^{\mathbf{b}}$ | Reference segment $^{\mathbf{b}}$ | Cardan sequence | Positive direction |
| :---: | :---: | :---: | :---: | :---: |
| Pelvis | Pelvis | Laboratory | Flex/ext - add/abd - int/ext rotation | Tilt - anterior <br> Obliquity - right down <br> Twist - right forwards |
| Hip* | Thigh | Pelvis | Flex/ext - add/abd - int/ext rotation | Flexion <br> Adduction <br> Internal rotation |
| Knee* | Shank | Thigh | Flex/ext - add/abd - int/ext rotation | Flexion <br> Adduction <br> Internal rotation |
| Ankle* | Foot | Shank | Flex/ext-add/abd-inv/ev rotation | Dorsiflexion <br> Adduction <br> Inversion |
| Virtual Ankle* | Virtual Foot | Virtual Shank | Flex/ext-inv/ev-add/abd | Dorsiflexion <br> Inversion <br> Adduction |

${ }^{\text {a }}$ Virtual segments are used for joint kinematics only.
${ }^{\mathrm{b}}$ Angles are calculated within the co-ordinate system of the reference segment.

## Table S5. System

| Capture system / software | Motion Analysis Corporation ${ }^{\text {a }}: 17$-camera Raptor/ Cortex version $6^{\text {a }}$ |
| :--- | :--- |
| Medium | Passive retro-reflective markers $: 12.7 \mathrm{~mm}$ with thin fabric base |
| Sampling frequency | 100 Hz |

Table S6. Processing

|  | Software |  |
| :--- | :---: | :--- |
| Eventing | Visual 3D $^{\mathrm{b}}$ | Kinematic algorithm (velocity-based, from ${ }^{4}$ ) |
| Filtering | Visual 3D $^{\mathrm{b}}$ | 7Hz-12Hz 4 4 ${ }^{\text {th }}$ order Butterworth, by marker ${ }^{5}$ |
| Interpolation | Cortex $^{\mathrm{a}}$ | Cubic spline / software-based virtual join ${ }^{\mathrm{a}}$ |

${ }^{a}$ Motion Analysis Corporation, Santa Rosa, CA, USA
${ }^{\mathrm{b}}$ C-Motion, Germantown, MD, USA
${ }^{\text {c }}$ Mathworks, Natick, MA, USA

## References

${ }^{1}$ Spoor CW. Rigid body motion calculated from spatial co-ordinates of markers. J. Biomech 1980; 13: 391-393.
${ }^{2}$ Hanavan Jr, EP. A mathematical model of the human body (No. AFIT-GA-PHYS-64-3). Air Force Aerospace Medical Research Lab Wright-Patterson Afb Oh, 1964.
${ }^{3}$ Harrington ME, Zavatsky AB, Lawson SE, Yuan Z, Theologis TN. Prediction of the hip joint centre in adults, children, and patients with cerebral palsy based on magnetic resonance imaging. J Biomech. 2007;40(3):595-602.
${ }^{4}$ Zeni Jr, JA., Richards, JG, \& Higginson, JS. Two simple methods for determining gait events during treadmill and overground walking using kinematic data. Gait Posture 2008, 27(4), 710-714.
${ }^{5}$ Giakas, G. Power spectrum analysis and filtering. Innovative Analyses of Human Movement, Champaign, IL: Human Kinetics, 2004.

